



Design and Optimization of an Optical Cavity to Interact with ⁸⁷Rb

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Introduction/Background

- I have been working on optimizing an optical cavity based on a new "photon counting" technique that will provide the necessary sensitivity to better detect weak signals.
- This apparatus, which will be able to distinguish between the desired signal and other sources of noise, utilizes an atomic cavity.
- Using atoms in a laser cavity, rather than just the laser cavity by itself, will reduce signal loss and improve the filtering of the incoming light.



Vermeulen et al., 2024

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Introduction/Background

- The readout method involves measuring the state of the valence electron of the Rb atom after its interaction with the IFO output signal.
- We want to increase the probability of an interaction between the incoming photon and an Rb atom.
- To do this, we will use a cavity that goes through a laser-cooled cloud of Rubidium atoms in a 4-mirror setup.
- Two of the mirrors will be curved in order to focus the incoming laser beam to as small a waist as possible.





- In practice, I used Finesse 3 to simulate the laser cavity.
- Given optical elements and path (assuming the beam is stable), it propagates the beam along its defined path, calculating important beam characteristics (w, w0, z, zR, and others).
- Parametrized by distance between mirrors and angle of incidence (AOI) (but with some assumptions to simplify geometry), as well as the mirror's radius of curvature (RoC).



- The waist depends on the angle of incidence.
- Ideally we want the AOI = 0° .
- The minimum angle of incidence is limited in practice by clipping.
- This means that the edge of the mirrors should far away from the propagating beam's center.
- Thus I approximated the segment from the center of the beam to the bottom of M1 and that from the bottom of M1 to its center to be parallel.



$$I(r,z) = I_0 \left[rac{w_0}{w(z)}
ight]^2 \exp \left[-rac{2r^2}{w^2(z)}
ight]$$

Steck, 2024

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- Given that constraint, the AOI was calculated using simple trigonometry:

$$\tan \theta_i = \frac{\Delta y}{L_1}$$
$$\theta_i = \arctan \frac{\Delta y}{L_1}$$
$$= \arctan \frac{20.2 \text{ mm}}{180 \text{ mm}}$$
$$= 3.20^{\circ}.$$

This produced the following beam in Finesse 3:

	z	w0	zr	W
L0.p1.o	0 m	900.52 um	1.6436 m	914.52 um
m3.p1.i	1 mm	900.52 um	1.6436 m	914.43 um
m3.p3.o	1 mm	900.52 um	1.6436 m	914.43 um
m4.p1.i	581 mm	900.52 um	1.6436 m	914.43 um
m4.p2.o	581 mm	900.52 um	1.6436 m	914.43 um
m1.p4.i	1.001 m	900.52 um	1.6436 m	980.95 um
m1.p3.o	1.001 m	22.891 um	1.0621 mm	980.95 um
N.p1.i	1.0465 m	22.891 um	1.0621 mm	22.891 um
N.p2.o	1.0465 m	22.891 um	1.0621 mm	22.891 um
m2.p1.i	1.092 m	22.891 um	1.0621 mm	980.95 um
m2.p2.o	1.092 m	900.52 um	1.6436 m	980.95 um
m3.p4.i	1.512 m	900.52 um	1.6436 m	914.43 um

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- Finally, I saw that there is astigmatism, which makes the waist size different depending on the axis.
- Thus, actual effective waist size is between that of each axis.

	Z	w0		
N.p1.i	1.0465 m	24.186 um		
N.p1.i	1.0465 m	22.891 um		

(d) Curved mirror, arbitrary incidence $R_e = R \cos \theta$ in the plane of incidence ("tangential") $R_e = R/\cos \theta \perp$ to plane of incidence ("sagittal")



Siegman, 1986

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- To interact properly with Rb, the light needs to be circularly polarized.
- However, planar cavities can only support one linear polarization at a time.
- Therefore, we will build a non-planar cavity that allows for circularly polarized light.
- Basic idea: non-planar cavities mix the linear polarizations.



- Unfortunately, Finesse 3 does not work well with non-planar cavity designs.
- Thus, we need to consider ray transfer (ABCD) matrices.
- In the 2d case we get a 2x2 matrix.



- In 3d, however, an additional axis introduces more elements, resulting in a 4x4 matrix.
- To do this, rotate into the frame of optical element, apply normal transformation, then reverse rotate back to original frame.
- To get the overall matrix, do this in series for all mirrors and multiply them in order.
- Off diagonal elements are hard to calculate as they involve the x-y cross-term effects.

$\begin{bmatrix} x_2 \end{bmatrix}$		$\int A_{xx}$	B_{xx}	$ A_{xy}$	B_{xy}	$\left[\begin{array}{c} x_1 \end{array} \right]$	Flaterin		
x_2'	n the th	C_{xx}	D_{xx}	C_{xy}	D_{xy}	x_1'	M_{xx}	M_{xy}	- overall 4×4]
y_2		$\overline{A_{yx}}$	B_{yx}	A_{yy}	B_{yy}	$\overline{y_1}$	$ig M_{yx}$	$egin{array}{c} M_{yy} \end{array}$	_ [matrix product]
$\begin{bmatrix} y'_2 \end{bmatrix}$		C_{yx}	D_{yx}	C_{yy}	D_{yy}	$\left\lfloor y_{1}^{\prime} \right\rfloor$			

Siegman, 1986

Future Work

- Finalize mirror spacing and radius of curvature
- Advance on non-planar cavity design
- Coordinate with suppliers for curved mirror production
- Analyze system robustness against errors (placement, misalignment, etc.)

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